large tetrabutylammonium cation, and spectral differences should vanish as they do.

Analogous solvent dependence of the stability of the trihalide ion is found in the literature on tribromide ion.²⁷⁻³³ This is consistent with the lit-

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2829 (1949)

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erature on solvent complexes of bromine which is parallel to that for iodine.34

The acid effect noted on the triiodide equilibrium, in the region of acidity 1 M HClO₄ is apparently the first evidence for a difference in the dissociation constants for HI and HI₃. The temperature variation in the peak extinction coefficient of triiodide is probably related to the origin of the absorption. This is a modified absorption of the iodide ion, which will be discussed elsewhere.

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Dissociation Pressures and Related Measurements in the System Aluminum Sulfate-Water¹

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Published data on the system aluminum sulfate-water are incomplete and contradictory. A static manometric method was used to measure the vapor pressures of known aluminum sulfate-water compositions at fixed temperatures as known quantities of water were withdrawn. Measurements were made at 25, 14 and 0°, and the sample size was varied. Equilibrium could be reached only for the higher hydrates. Within the range of conditions studied both of the compounds $Al_2(SO_4)_3$. 16- H_2O and $Al_2(SO_4)_3$. 17H₂O appear to exist and are, furthermore, mutually soluble. The 17H₂O is thus capable of losing up to one mole of zeolitic water. Dissociation pressures for the systems vapor-liquid-17H₂O and vapor-16H₂O-lower hydrate, and eutectic point were redetermined giving results markedly different from the only previous values. The solubility curve of the 17H₂O was extended. Melting points of hydrated aluminum sulfate in various stages of hydration indicated transition temperatures at ~111° and ~128°. Previous boiling point elevation values have been improved upon and extended to higher the subscience of the standard curve of the standard curve in the subscience of the standard curve in the subscience of hydration values have been improved upon and extended to higher the subscience of the subscience of the standard curve of the standard curve of the subscience of the standard curve of the subscience of the standard curve of the standard curve of the standard curve of the transition temperatures at ~111° and ~128°. Previous boiling point elevation values have been improved upon and extended to higher the subscience of the standard curve of the standard curve boiling point elevation values have been improved upon and extended to higher to concentrations. higher concentrations.

The phase relations in the system aluminum sulfate-water are, surprisingly, not well established considering the widespread use of the hydrates. There is, for instance, no complete agreement as to the identity of the highest hydrate² although the existence of (1) a hydrate or hydrates with 18, 17 or 16 moles, and (2) a hydrate with 10 or 9 moles of water of hydration is generally conceded. Smith and others³ showed the highest hydrate at 25° to be the 17 but Bassett and others⁴⁻⁶ still regard it as the 16 (see Discussion). The second highest hydrate would appear to be the 10 from the work of Gee⁷ but 9 from that of Henry and King.² If, as Gee claims, the highest hydrate is the 10 (or 9) at 80° but the 16 at 30° there should be a break in the aqueous solubility curve between these two temperatures. This is not evident in the measurements of Taylor and Bassett.⁶ Furthermore, the only published boiling point elevation data8 were obtained by the crudest of methods, the authors themselves suggesting that their measurements be repeated.

(1) Presented before the Division of Physical and Inorganic Chemistry of the American Chemical Society at Chicago, Ill., September, 1953.

(2) Cf. J. L. Henry and G. B. King, THIS JOURNAL, 71, 1142 (1949). (3) N. O. Smith, ibid., 64, 41 (1942); H. A. Horan and J. A. Skarulis, ibid., 61, 2689 (1939); W. F. Ehret and F. J. Frere, ibid., 67, 68 (1945).

(5) H. Bassett and W. Watt, *ibid.*, 1408 (1950).

(6) D. Taylor and H. Bassett, ibid., 4431 (1952).

(7) E. A. Gee, This Journal, 67, 179 (1945).

(8) W. L. Badger and J. S. France, Ind. Eng. Chem., 15, 364 (1923).

Dissociation Pressures

To resolve the problem of the identity of hydrates it would appear that isothermal measurements of the equilibrium pressure of the system as water is gradually withdrawn would provide the best means, by noting the compositions of solid at which marked changes in pressure are observed. Such dissociation pressure measurements at 20° are described by Kremann and Hüttinger⁹ using equilibration over sulfuric acid solutions, and the hydrates 18, 16, 12 and 2 were claimed. Their results are open to alternative interpretations, however, and their pressures do not agree with those reported below. Taylor and Bassett⁶ give a brief reference to dissociation pressure measurements at 25° using a static manometric method. Equilibrium was approached from the direction opposite¹⁰ to that used by us and their results differ from, and are less complete than, ours.

Experimental

In the present work pressures were measured by a method patterned after that of Logan.¹¹ The sample (A, Fig. 1) was contained in a thermostated 50-ml. glass bulb B leading directly to one arm of a mercury manometer C. The other arm led to a Hyvac pump and McLeod gage, and to a means of introducing or removing measured quantities of water. Air-free water was introduced by drawing water into E (previously evacuated) through F, boiling out the air through

⁽⁴⁾ H. Bassett and T. H. Goodwin, J. Chem. Soc., 2239 (1949).

⁽⁹⁾ R. Kremann and K. Hüttinger, Jahrb. k.k. Geol. Reichsanstalt, 58, 637 (1908).

⁽¹⁰⁾ Private communication.

⁽¹¹⁾ T. S. Logan, J. Phys. Chem., 36, 1035 (1932),



F and then distilling into the calibrated tube D where the depth gave a measure of the quantity. It was then distilled into A. Tube D was used similarly to measure

amounts of water withdrawn from A. By maintaining a negligible pressure on the right arm of the manometer, as shown by the McLeod gage, the differences in level, measured with a Gaertner cathetometer to 0.01 mm., gave the pressure of the system directly.

The aluminum sulfate was prepared from pure aluminum and sulfuric acid and recrystallized.4 To remove free acid it was heated to intumescence, ground and heated in vacuo at 170° Analysis of this product gave the following results: $96.86\% \text{ Al}_2(\text{SO}_4)_3$ by aluminum¹² and $96.80\% \text{ Al}_2(\text{SO}_4)_3$ by sulfate¹³ anal-No basic salt was present, therevsis. fore. This material was dissolved in water, sealed into the apparatus at A, excess water removed with suction and was then heated for two days at 170° under vacuum to degas. Higher tem-peratures decompose the sufference peratures decompose the sulfate to the oxide. This technique utilized the intumescent character of the substance to produce a porous degassed sample with-

out loss of sulfur; when so prepared it showed no tendency to fill the apparatus with dust when heated.

More than enough water to hydrate the material fully was now admitted and the pressure measured after withdrawal of small measured amounts of water. At the conclusion of the run the residue in B was analyzed and the composition for each observed pressure calculated. In contrast to the findings of Taylor and Bassett¹⁰ equilibrium appeared to be readily obtainable only on dehydration and not on hydration, and, even then, only for higher water content of solid. Measurements were conducted with varying sample weights at 25°, 14° and 0° ± 0.03. Figure 2 gives the resulting pressures, corrected to 0°, for the corresponding total compositions of solid phase. Points marked with a vertical arrow are not reliable, as the pressure was still rising very slowly.

Discussion of Results

At all three temperatures the data indicate approximate initial constancy of pressure as water is withdrawn followed by a *gradual* drop in pressure to a new approximately constant value. This constancy was much better in some runs than in others. In all but run 3 the drop in pressure (12) I. M. Kolthoff and E. B. Sandell, THIS JOURNAL, **50**, 1900 (1928).

(13) Reference 4, p. 2242.

began at a solid composition of about 52.8% and ended at about 54.0% Al₂(SO₄)₃. Inasmuch as the calculated compositions of the $17H_2O$ and $16H_2O$ are 52.76% and 54.27% Al₂(SO₄)₃, respectively, the existence of both of these compounds is indicated. The higher constant value refers, then, to the system vapor-liquid-17H₂O and the lower to the system vapor- $16H_2O-xH_2O$ where " xH_2O " is the next lower hydrate which was not identified in this study because attainment of equilibrium required a prohibitive time for lower water contents. The gradual drop in vapor pressure shows that the 17H₂O is capable of losing up to one mole of water present as solid solution. It may be argued that the 16H₂O is a true compound, but that the fact that the upper limit of solid solution corresponds to the stoichiometric composition of 17H₂O is merely a coincidence; it should be observed, however, that the correspondence was found at all three temperatures. Within the range of conditions studied, then, the 17H2O has the phase behavior of a compound. As essentially the same



Fig. 2.—Variation of pressure of water vapor with over-all composition of solid.

results were obtained with different sample weights at 25° the possibility of accounting for the additional mole of water in terms of adsorption^{4,6} seems to be ruled out. In run 3 the drop in pressure occurred between 51.0% and 53.0% Al₂(SO₄)₃ caused by what is believed to be a non-uniform sample. The latter was unusually large and portions of it may well have been protected from dehydration. In spite of this, the pressure values, if not the compositions, are believed to be dependable. It may be noted that this larger sample gave a better lower constant pressure, as would be expected.

The highest hydrate in equilibrium with saturated solution is, then, the $17H_2O$, in agreement with previous workers. (This is substantiated further by a fourth run at 25° (not shown) using 1.6 g. of $Al_2(SO_4)_3$ in which the sample was removed and analyzed directly when the pressure of the system just began to fall below that of the higher level. Its composition was 52.6% $Al_2(SO_4)_3$.) Over the range of conditions studied both the 16- and $17H_2O$ appear to be chemical individuals and form a complete series of solid solutions in each other. It is seen, further, that the composition of the hydrated material is especially sensitive to prevailing humidity conditions and this probably accounts for the lack of agreement among the various investigators as to its composition.

Bassett and co-workers,^{4,6} on the other hand, assign to the saturating phase at 25° the formula Al₂(SO₄)₃·16H₂O while admitting that its composition can vary between that of the $16H_2O$ and the 17H₂O. The claim for the 16H₂O is made by Bassett and Goodwin from a study of the system Al_2O_3 - SO_3 - H_2O at 25° for the following reasons: (a) In the appropriate isothermally univariant region "all the tie-lines come very close to the point" for that composition, (b) all the solid phases so obtained have the same appearance and X-ray pattern, and (c) the solid obtained at higher acid concentrations showed no change when kept over more dilute acid solutions. Referring to (a) the quotation above is true if one considers only those tie-lines where the acid concentration in the saturated solution is high enough to give results of significance, but the tie-lines in Taylor and Bassett's paper,⁶ for what is essentially the same situation (but extended to nearly 50% H₂SO₄), actually run (on the average) closer to the point for $17H_2O$ than for 16H₂O. Concerning (b) it is entirely possible that the extra zeolitic water would not make a detectable alteration in the appearance or the X-ray pattern. Observation (c) is in harmony with our experience that, except for the lowest hydrates, hydration proceeds with great difficulty in the absence of direct contact with a liquid phase.



Fig. 3.—Variation of dissociation pressure with temperature.

In order to obtain the isothermally invariant pressures represented by each horizontal in Fig. 2 all the values which seemed to refer to the given horizontal were averaged, yielding the results shown in Table I. The numerals in parentheses refer to the number of readings averaged.

	Invariant Pressures (Mm.)			
	Uppe r horizontal	Lower horizontal		
25°	$20.6 \pm 0.1(9)$	$5.0 \pm 0.5(10)$		
14°	$10.4 \pm 0.1(3)$	$1.73 \pm 0.34(4)$		
0°	$3.95 \pm 0.02(5)$	$0.58 \pm 0.10(4)$		

In runs 1, 4 and 5 it was possible to obtain a few data from the direction of hydration rather than dehydration by distilling into the system a small quantity of water immediately after the last point for the dehydration had been obtained. The resulting pressures were constant for only an hour or two, but seemed to be significant. They are recorded in Table II.

TABLE II

Metastabi	METASTABLE DISSOCIATION PRESSURES					
	<i>P</i> , mm.	Wt. % Al ₂ (SO ₄):				
Run 1 (25°)	10.9 ± 0.7^{a}	54.72				
Run 4 (14°)	4.85 ± 0.40	55.60				
Run 5 (0°)	1.65 ± 0.20	54.79				

 a Three earlier exploratory runs had yielded the values 10.3, 10.9, 10.6 mm.

In view of the method whereby they were obtained they are believed to represent metastable equilibria for the system vapor-liquid- xH_2O . They refer probably to the same equilibria which Taylor and Bassett⁶ describe as the system vapor-14H₂O-16H₂O. The probable error in the above pressure values is unknown, but estimated to be that shown.

Dissociation pressures of the following isothermally invariant systems were thus obtained: vaporliquid-17H₂O, vapor-16H₂O-xH₂O and vapor-liquid -xH₂O (?). A plot of log P vs. 1/T (Fig. 3) gives straight lines, the slopes of which lead to the following mean values of ΔII (per mole of water vapor formed)

I.iquid
$$\rightleftharpoons$$
 Al₂(SO₄)₃·17H₂O(s) + vapor; $\Delta H \doteq 10,700$ cal. ± 50

Liquid \swarrow Al₂(SO₄)₃·xH₂O(s) + vapor; $\Delta H = 12,400$ cal. ± 2000

Al₂(SO₄)₃·16H₂O(s) \longrightarrow Al₂(SO₄)₃·xH₂O(s) + vapor; $\Delta H = 14,300$ cal. ± 2000

The slope for the first of these three systems is indistinguishable from that for the system $H_2O(l) \rightleftharpoons$ $H_2O(v)$, also included in the figure along with the sublimation curve of ice.

Solid-Liquid Equilibria.—The only published measurements of the freezing points of aqueous aluminum sulfate solutions are those of Kremann and Hüttinger⁹ and it seemed desirable to repeat them. Mallinckrodt hydrated material (Analytical Reagent) was dissolved, cooled to 0°, stirred with ice in a Dewar flask and the final temperature recorded to $\pm 0.1^{\circ}$. Samples of the liquid were withdrawn for analysis giving the following results which are included in Fig. 4

Wt.
$$\%$$
 Al₂(SO₄)₃06.3716.2023.927.2Freezing point0 -0.8 -3.3 -9.6 -12.0 (°C,)(eutectic)

These freezing points are lower than those found by Kremann and Hüttinger especially for the higher concentrations. (Their value for the eutectic was 23.4% and -4.0° .) The solid phases are ice and Al₂(SO₄)₃·17H₂O. There is, therefore, a quadruple point (ice + 17H₂O + liq. + vap.) at -12° and 1.63 mm.

The smoothed solubility curve for the hydrated salt is also shown in Fig. 4. It is drawn through

the recent values of Taylor and Bassett⁶ and those of Horan and Skarulis³ and the authors. The latter obtained their data by rotating sealed glass-stoppered tubes containing excess salt and water in a thermostat and removing samples for aluminum analysis by a pipet. Our figure for 25° agrees well with that of Taylor and Bassett (not shown). Some data of Henry and King² are also shown for comparison. We believe our solubility figure for 80.6° (37.4% Al₂(SO₄)₃) may be too high because of possible loss by evaporation during sampling, but our purpose was chiefly to decide whether the stable solid phase at this temperature is highly hydrated or

not. The solid was separated by decanting off the liquid phase and rapidly blotting to near dryness. Analysis of it showed 48.0% Al₂(SO₄)₃ so that it could hardly be the $10H_2O$ (65.5% Al₂(SO₄)₃) at 80° as claimed by Gee.⁷ Apart from this no other solid phase analyses were conducted for: (a) the solid phase at 25, 14 and 0° had already been established in the dehydration experiments described above, (b) the smoothness of the solubility curve in Fig. 4 from the eutectic to 110° made a change of solid phase unlikely, (c) the $17H_2O$ was found to undergo no melting below about 110° . The solid phase for the entire temperature range is, therefore, the $17H_2O$. The very small temperature coefficient of solubility from -12° to above room temperature is noteworthy.

In an attempt to extend the measurements to higher temperatures where high viscosity becomes a problem, the melting point approach was used. Ground samples of recrystallized hydrate, brought to various stages of dehydration by heating at 90°, were analyzed and melted in sealed capillaries. The precise temperatures of initial and, particularly, of final melting were difficult to observe, but the results indicate transitions at $\sim 111^{\circ}$ and, possibly, $\sim 128^{\circ}$. The exact phase relations of the liquid 17- and 16H₂O above 100° are not yet clear. Taylor and Bassett⁶ are similarly in doubt. Nevertheless, the 17H₂O prepared carefully in the apparatus of Fig. 1 melted at 109.0–111.5°.¹⁴ It is

(14) Cf. the value of ~114° for the mineral alunogen, Al₂(SO₄)₃:x-H₂O, quoted by J. D. Dana, "The System of Mineralogy," 7th Ed., Vol. 2, John Wiley and Sons, Inc., New York, N. Y., p. 538.

difficult to say whether this is congruent or incongruent melting. Mixtures richer than about 60% had not melted completely at 200°.

Liquid-Vapor Equilibria.—In order to improve on the previous boiling point values for aqueous aluminum sulfate solutions boiling points were redetermined at 763 mm. ± 1 using Analytical Reagent grade material and a Cottrell apparatus. The solutions were analyzed subsequent to boiling.



Fig. 4.--Temperature-concentration relations in the system Al₂(SO₄)₃-H₂O.

For the more concentrated solutions higher boiling points were obtained than found earlier.⁸ A discolored, but clear and very viscous, solution heated under reflux without the Cottrell pump, boiled steadily at 123° in contact with a solid phase (not identifiable). The liquid composition was 60.4% Al₂(SO₄)₃. While the possibility of appreciable hydrolysis is not ruled out it seems unlikely at such high concentrations, for no loss of sulfuric acid occurs on heating the hydrate in air to several hundred degrees. The data obtained are given below and included in Fig. 4

Wt. % Al ₂ (SO ₄) ₃	0	21.1	41.4	60.4
B.p. at 763 mm., °C.	100.1	101.1	106.3	123

Many of the above results are collected in Fig. 4, including the temperature of initial and final melting of $Al_2(SO_4)_3 \cdot 17H_2O$. It is of interest to note that the latter substance $(52.8\% Al_2(SO_4)_3)$ finishes melting at a temperature just below that of the boiling point of a liquid of that composition. This unique juxtaposition of melting and boiling points combines with the viscous character of the melt to give the hydrate its property of intumescence.

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